## **Droplet** formation

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Grenoble experiment



Descamps et al, 2008 Matas et al., 2011 Jérôme et al, 2013 Fuster et al, 2013 Ling et al, 2015

and of course Hopfinger, Lasheras, Cartellier, Villermaux, Hoepffner, Popinet, Boeck, Rossi ...









# I) Is it possible to do a real Direct Numerical Simulation of atomisation, resolving all the scales ?

2) What can we learn from these very detailed simulations ?







#### I) 2D flows

2) 3D flows









#### 2D simulations of the planar « Grenoble » setup.



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The Grenoble quasi 2D experiment set up



Navier-Stokes equations with interfaces

$$\partial_t(\rho \mathbf{u}) + \nabla \times (\rho \mathbf{u} \mathbf{u}) = -\nabla \rho + \nabla \times (2\mu \mathbf{D}) + \sigma \kappa \delta_s \mathbf{n} + \rho \mathbf{g},$$

where the strain-rate tensor is:

$$D_{ij} = \frac{1}{2} \left( \frac{\partial u_j}{\partial x_i} + \frac{\partial u_i}{\partial x_j} \right),$$

and both fluids are considered incompressible

$$\nabla \cdot \mathbf{u} = 0$$
.

Compressible fluids: possible but difficult and less relevant.







## Surface tension

Treatment of surface tension by Continuous Surface Force (« CSF » method, Brackbill, Kothe and Zemach JCP 1993)

σκ **n**
$$\delta_s$$
 ≈ σκ <sup>h</sup> $\nabla^h C$ 

Many methods for  $\kappa$  .









#### Use Gerris flow solver (S. Popinet) with adaptive oct-tree and quad-tree grids











Navier-Stokes with variable minimum grid size according to a subdivision of the computational domain.







Simulation with a separator plate at density ratio (1/r = 100)



Movie by Daniel Fuster and Jérôme Hoepffner using the Gerris Flow solver



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Simulation with a separator plate at density ratio (1/r = 100)

т	r	$Re_{g}$	$Re_l$	$We_{g}$	$We_l$	M
0.017	0,01	2640	290	19	8	2,4

Movie by Daniel Fuster and Jérôme Hoepffner using the Gerris Flow solver



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Compare to experiments in Grenoble (Cartellier, Matas) . Flow from right to left. Video with help of Jérôme Hoepffner and Jon Soundar.



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Compare to experiments in Grenoble (Cartellier, Matas) . Flow from right to left. Video with help of Jérôme Hoepffner and Jon Soundar.







We need linear theory for spatially developping flows.

For that, we need to know what are absolute and convective instabilities !









Convective/absolute instabilities

 Absolute: a spatially localized perturbation at x=0 and t=0 grows in the entire space



corresponds to a well-defined oscillator frequency in the entire domain, a so-called « global mode »



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Convective/absolute instabilities

2) Convective instability: a spatially localized perturbation at t=0 is convected downstream with the flow



No single frequency is observed but instead, broadband noise is seen. The system is seen to be a noise amplifier. Upstream turbulence matters



So what does linear theory say about our problem ? Is it convective or absolute ?

Linear theory has an enormous dependence on the wake flow correction.





Simplified base flows









## Most important parameter: momentum flux ratio (or ratio of dynamic pressures)

$$\boldsymbol{M} = \frac{\rho_g \boldsymbol{U}_g^2}{\rho_l \boldsymbol{U}_l^2}$$









Grenoble experiments: Cartellier, Matas, Marty



#### Now the ultimate test ! Compare :

- Experiments
  - Numerics
- Linear theory











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Primary instability of sheared interfaces is still a challenge however.



Strong influence of the turbulence level on the measured frequency. Figure from Cartellier & Matas (LEGI)





2) 3D: How do 2D sheets break into 3D ligaments and droplets ?







How do 2D sheets break into 3D ligaments and droplets ?

Two universal mechanisms:

I) Cylinder (rim) + Rayleigh-Plateau instability



Dombrowski and Johns (1983) Zhang, Li V., Brunet, P., Eggers, J. & Deegan, R. D. 2010

2) Hole formation



Roisman et al (2006)







Other more specialized mechanisms

for atomization streamline vortices pre-existing in the upstream bour



 Non-normal instability of two phase mixing layers (Yecko & Zaleski 2005) (Squire theorem does not apply in two-phase situation, the non-normal instability also leads to streamwise vortices)

#### for splashing

- Richtmyer-Meshkov instability (Gueyffier & Zaleski 1998)









## What is observed in atomization ?









#### 2D waves + attached ligaments formation





Photograph: Alain Cartellier and Jean-Philippe Matas

#### Holes + fishbone patterns



Photograph: Ludovic Raynal



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## "A20" simplified case (Stanley Yue Ling) dimensional values

	Density (ρ) Kg/m³	Viscosity (µ) Pa-s	Surface Tension (σ) N/m	Jet Height (H) mm	Boundary Layer (δ) mm	Injection Velocity (U) m/s
Gas	50	5E-05	0.05	0.8	0.1	10
Liquid	1000	1E-03	0.05	0.8	0.1	0.5



## "A20" Benchmark: dimensionless values

Μ	$Re_{g,\delta}$	Re <sub>g,H</sub>	We <sub>g,δ</sub>	r	m	V
$\frac{\rho_g U_g^2}{\rho_l U_l^2}$	$rac{ ho_g U_g \delta}{\mu_g}$	$rac{ ho_g U_g H}{\mu_g}$	$rac{ ho_g U_g^2 \delta}{\sigma}$	$rac{ ho_l}{ ho_g}$	$rac{\mu_l}{\mu_g}$	$rac{U_l}{U_g}$
20	1000	8000	10	20	20	20



- Turbulent gas flow
- Convective instability Fuster et al. 2013, Otto et al. 2013
- "Strong" atomization

## Simulation Cases

Domain: Lx=16H, Ly=8H, Lz=2H; End-Time: t/(H/Ug)=400

Cases	h(µm)	H/h	# of cells	# of time steps	Total CPU time (hr)
МО	25	32	8.4 Million	4.9E+04	2.5E+03
M1	12.5	64	67 Million	1.0E+05	4.3E+04
M2	6.25	128	537 Million	2.2E+05	5.0E+05
МЗ	3125	256	4 Billion	4.5E+05	8.0E+06

CPU time estimate based on performance on TGCC-CURIE machine














#### Sheet and rim formation dynamics





#### DB: multi00160.root Cycle: 0 Time:0.016

DB: multi00160.root Cycle: 0 Time:0.016









































#### Interfacial wave interaction













Ligaments formation due to (a) fingering from the tip of liquid sheet and (b) hole formation in the liquid sheet. The color on the interface indicates the streamwise velocity.











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I) Is it possible to do a real Direct Numerical Simulation of atomisation, resolving all the scales ?

#### Not yet

2) What can we learn from these very detailed simulations ?

How to look at the experiment again (mechanisms much more complex than expected).









#### Acknowledgement







Y. Ling, D. Fuster, G Tryggvason, S. zalesk "Spray formation: an inverse cascade", <u>arXiv:1511.04234</u>



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### **Backup Slides**

This simulation is

- slow

- unstable

- does not parallelize properly

- does not have Lagrangian particles

Challenge: do better.

Two approaches:

- a much more efficient approach to computing on octree: Basilisk by S. Popinet: http://basilisk.fr
- 2) or a very simple code on regular grids: Parissimulator by Scardovelli, Ling, Tryggvason, Zaleski http://parissimulator.sf.net









Speed issues



Friday, June 17, 16







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Add Lagrangian Point Particles (LPP) that obey a point-particle equation

$$\frac{\mathrm{d}\mathbf{u}_{\rho}}{\mathrm{d}t} = \mathbf{F}_{\rho} \left[\mathbf{u}_{\rho}, \mathbf{u}_{f}(\boldsymbol{x})\right]$$

The force is determined by the surrounding carrier fluid velocity field  $\mathbf{U}_{f}(\mathbf{x})$ It reacts on the Navier-Stokes equation through a smoothing Kernel G :

$$\rho$$
D**u** / Dt = - $\nabla p$  +  $\nabla \times (2\mu \mathbf{D})$  + σκδ<sub>s</sub>**n** - **F**<sub>p</sub> \* **G**

where the strain-rate tensor  ${f D}$  is

$$D_{ij} = \frac{1}{2} \left( \frac{\partial U_j}{\partial x_i} + \frac{\partial U_i}{\partial x_j} \right).$$







The choice of resolved interface or LPP modelling depends on the type of simulation and on grid resolution









#### VOF to LPP conversion - High Reynolds - CORIA (Berlemont) jet



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## **Total Gas Kinetic Energy**



# **Total Liquid Kinetic Energy**



## **Total Interfacial Area**



## Enstrophy





### Interfacial Wave Evolution

#### 2D Slice of interface from t=19.0-21.9m



### Self-Similar Wave



## **Averaging Velocity**

#### m0



m1





# **Averaging Interfacial Area**

#### m0



#### m1





## **Turbulence Fluctuations**



## **Energy Spetra**



### Interfacial Instability

m1

m0





Same as before, higher resolution (Pascal Ray)

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Same as before, higher resolution (Pascal Ray)

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nswc














### The iconic Marmottant-Villermaux case



injection diameter D = 7.8 mm

 $\operatorname{Re}_{g} = 16000, \operatorname{We}_{g} = 200$ based on D<sub>1</sub>

Simulation : Two months on 64 AMD processors

line of eight 512<sup>3</sup> boxes – (equivalent regular mesh but we use octree adaptation)

Difficult to go to higher levels of refinement













Boundary layer size 157 µm

Injector thickness comparable.









Simulation: Gilles Agbaglah











Simulation: Gilles Agbaglah













experimental and computed at UPMC

$$u_2 = 35 \text{ m} / \text{s}$$







Planar shear flow of Descamps, Matas & Cartellier. 2nd colloque INCA, 2008.

Particle trajectories are measured.

 $\text{Re}_{\delta}$  = 1000

Simulation  $64 \times 256 \times 512$ 





























Refinement level  $I.D/\Delta x=15$ . Spurious currents observed.

Kinetic energy of the droplet











## Refinement level 2. $D/\Delta x=30$ . Kinetic energ



Refinement level 2.  $D/\Delta x=30$ . Kinetic energy of the droplet











## diameter d=8 mm

### DB: multi00001.root Cycle: 0 Time:0.0002 Contour Var: cvof 0 -2 4 6<sup>-10</sup> (x10<sup>--3</sup>) - 0.5000 Max: 1.000 Min: 0.000 Pseudocolor Var: vor\_y -3.519e+04 Ò 6<sup>min (x10^-3)</sup> 8 10 0 - 1.756e+04 --72.81 ~-1.771e+04 -3.534e+04 Max: 3.519e+04 Min: -3.534e+04 Auto (x10\*-3) х 0 z user: tomasarrufat Mon Mar 9 14:43:12 2015

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diameter d=8 mm











- Even for  $D/\Delta x = 60$  the boundary layer is only covered by 5 cells.

- The boundary layer is very small relative to the droplet diameter.

- Such results suggest that the accurate solution of air flow with water droplets can be extremely challenging.









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# experiments by Thoroddsen









## Even higher resolutions, with octree-AMR, up to D/h $\sim$ 6000.



Adapting on curvature and (less strongly) on vorticity







Thoroddsen, Thoraval & others + Gerris, KAUST, Phys. Rev. Lett. (2012)

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## Figure 4f









Figure 4f

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