

# The turbulent/non-turbulent interface in a plume

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with

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# The stars



Henry Burridge



Jamie Partridge



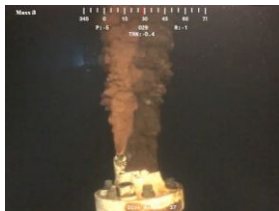
David Parker



Emily Kruger



# Plumes in the environment



## Part I

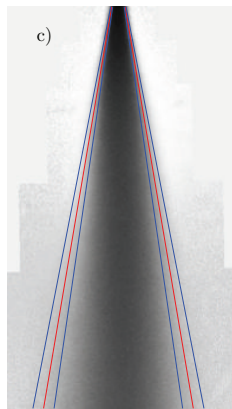
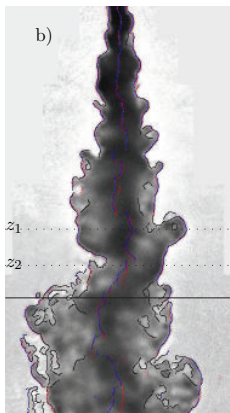
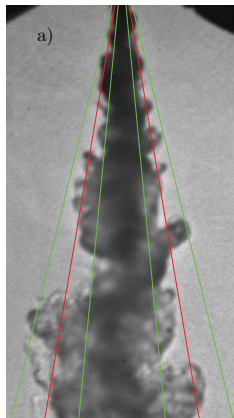
- 1 Can we determine the buoyancy flux in a plume from visual observations?
- 2 How is the speed of observable structures related to the speed in the plume?

## Part II

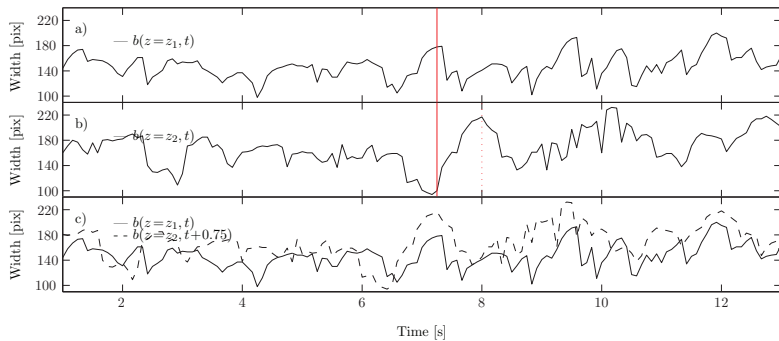
- 1 What is the flow in the ambient fluid outside the plume?
- 2 How is this fluid entrained?
- 3 Why is the average buoyancy width greater than the velocity width?

# Laboratory shadowgraph

# Shadowgraph images



# Time series



# Plume equations

Volume flux  $Q = 2\pi \int_0^\infty r w(r, z) dr$

Momentum flux  $M = 2\pi \int_0^\infty r w(r, z)^2 dr$

Buoyancy flux  $F = 2\pi \int_0^\infty r w(r, z) g'(r, z) dr$

Plume equations Morton, Taylor & Turner 1956

$$\frac{dQ}{dz} = 2\pi^{1/2} \alpha M^{1/2} \propto 2\alpha b w, \quad \frac{dM}{dz} = \frac{QF}{M} \propto b^2 g', \quad \frac{dF}{dz} = 0,$$

Entrainment constant  $\alpha$



# Plume scales

Volume length  $L_Q = \frac{Q_0}{M_0^{1/2}},$

Jet length  $L_M = \frac{M_0^{3/4}}{F_0^{1/2}} = \sqrt{\frac{8\alpha_T}{5}} \frac{L_Q}{\Gamma_0^{1/2}},$

Plume parameter  $\Gamma = \frac{5}{8\alpha_T} \frac{Q^2 F}{M^{5/2}},$

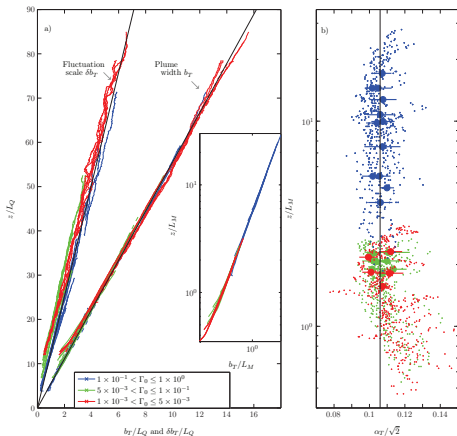
Pure plume  $\Gamma_0 \sim 1$

Moderately forced  $\Gamma_0 \sim 0.1$

Forced  $\Gamma_0 \sim 0.01$

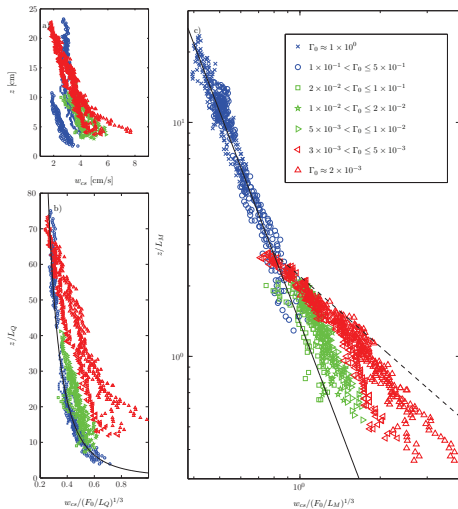
# Plume width

Pure plume    Moderately forced    Forced

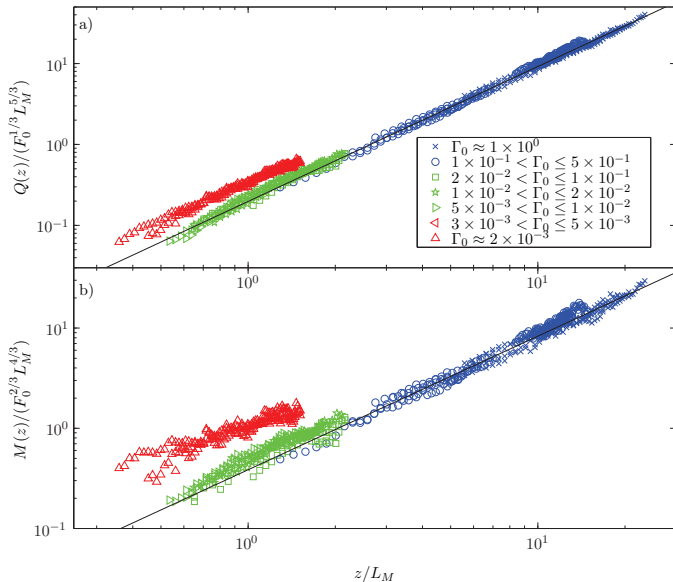


Entrainment constant  $\alpha_T = 0.106\sqrt{2}$

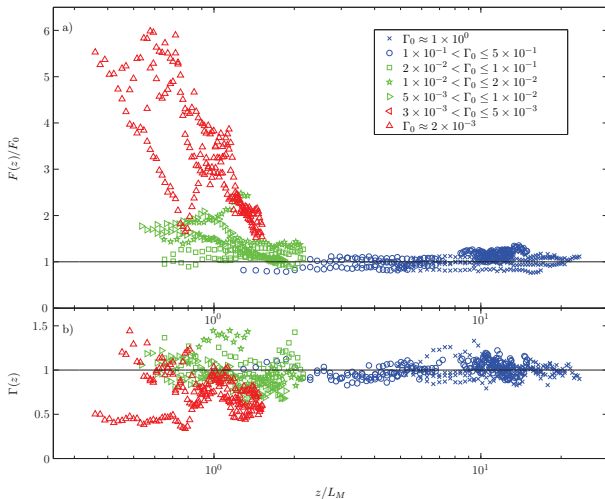
# Vertical velocity scaling



# Volume flux



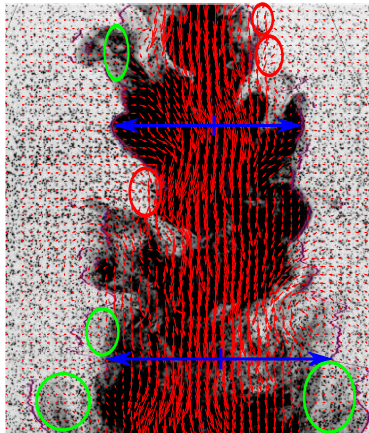
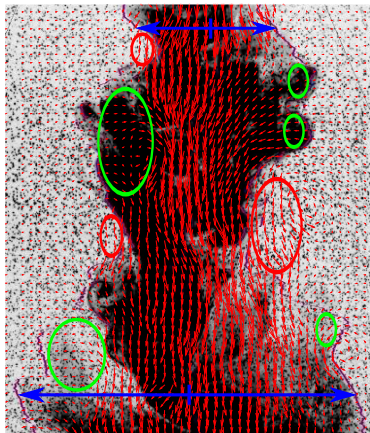
# Buoyancy flux and plume parameter



- Velocity of coherent structures is 30% of centreline velocity (60% of top-hat velocity)
- Motion of visible coherent structures on the edge of a plume can be used to predict the buoyancy (15%) and volume (5%) in a pure plume

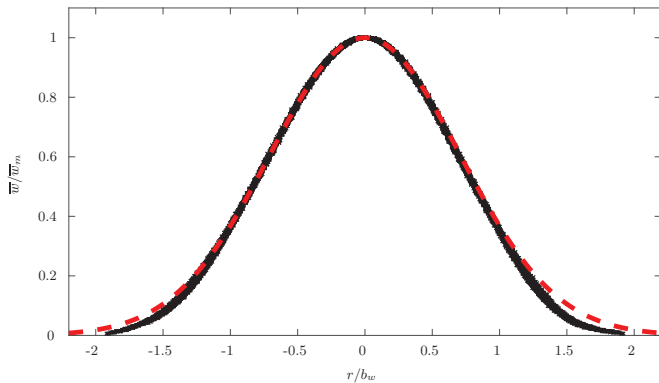
# Planar video

# Structures

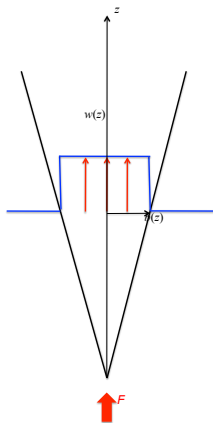




# Velocity profile - Gaussian



# Top-hat variables



$$\overline{w(r, z)} = \frac{1}{T} \int_0^T w(r, z, t) dt$$

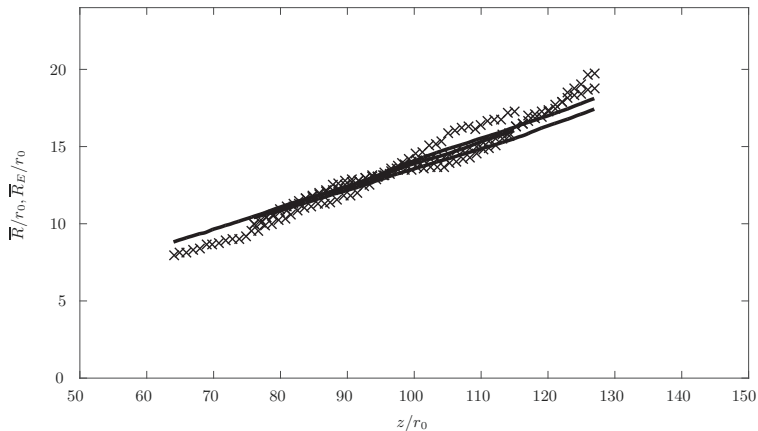
$$\overline{Q} = \int_{-\infty}^{\infty} r \overline{w(r, z)} dr$$

$$\overline{M} = \int_{-\infty}^{\infty} r \overline{w(r, z)}^2 dr$$

$$\overline{R} = \frac{\overline{Q}}{\overline{M}^{1/2}}$$

$$\overline{W} = \frac{\overline{M}}{\overline{Q}}$$

# Plume width



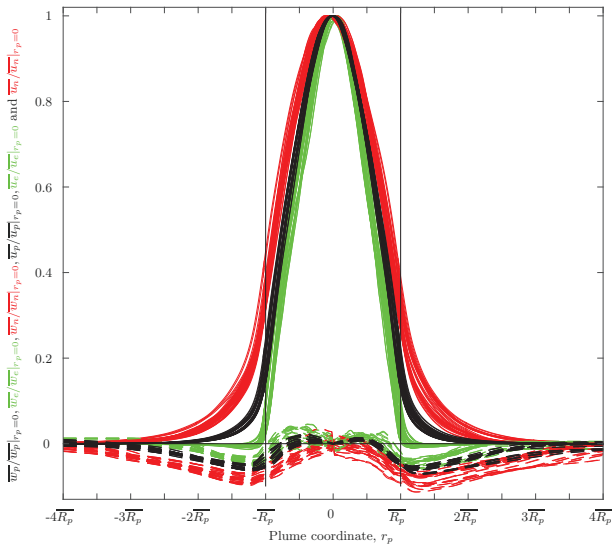
Crosses are edge values, lines are flux values

# Conditional velocities

Time average

Eddies present

Eddies absent

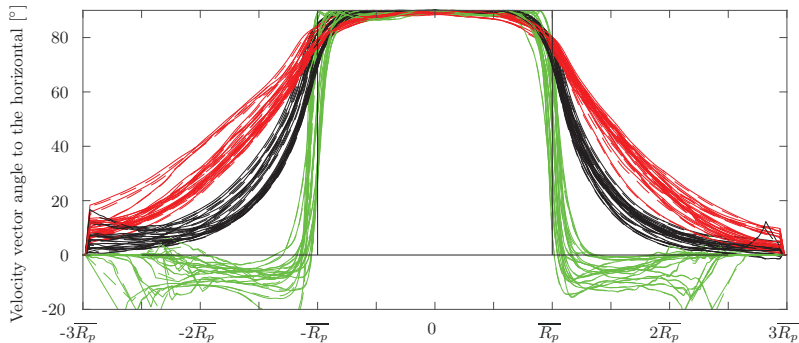


# Conditional angles

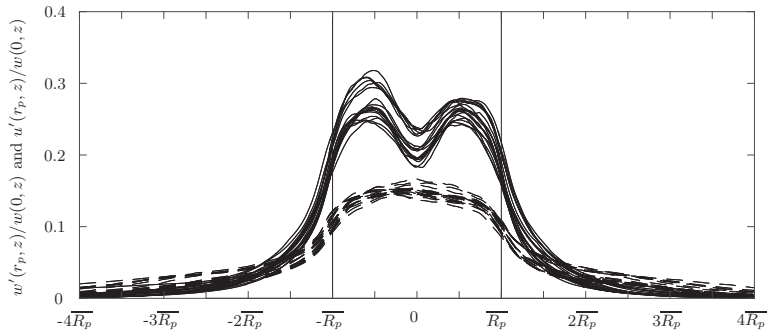
Time average

Eddies present

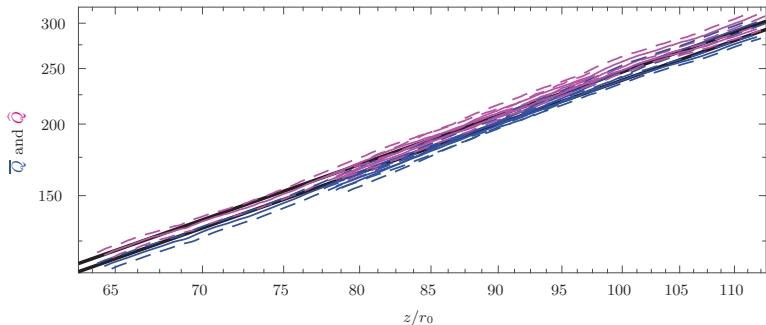
Eddies absent



# RMS fluctuations



# Volume fluxes



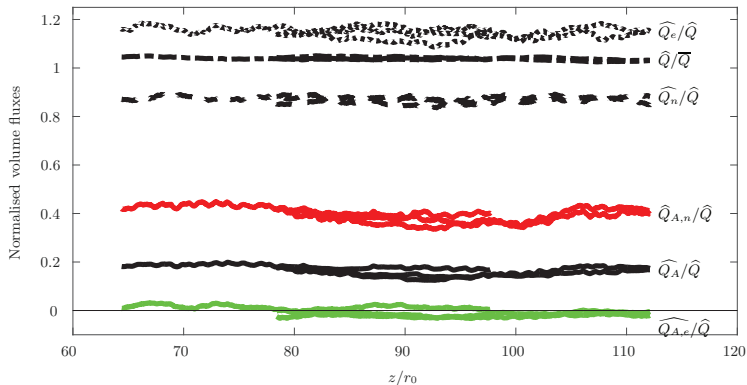
$$\hat{Q} = \frac{1}{T} \int_0^T \int_{-\infty}^{\infty} r_p w(r_p, z, t) dr_p dt$$

# Volume fluxes

Time average

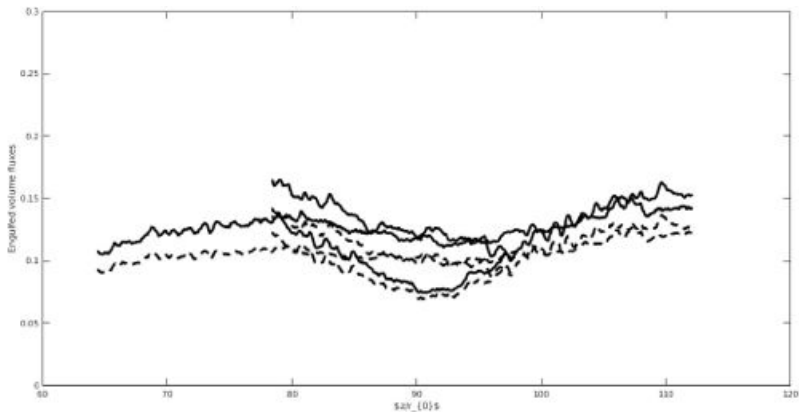
Eddies present

Eddies absent



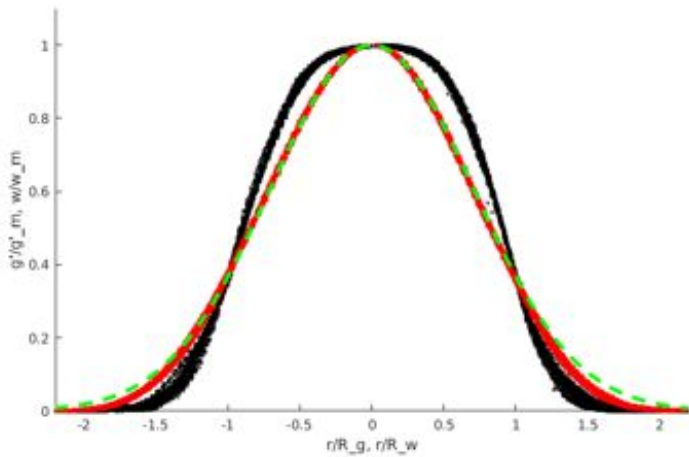


# Engulfed fluid

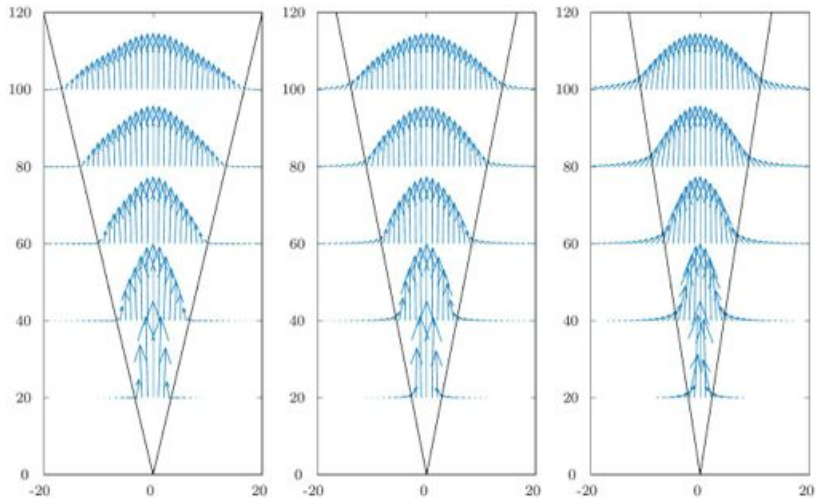


About 10 – 15 % of fluid in plume is engulfed

# Average fields



# Average flow fields



# 3D tomography

# Conclusions

- Velocity of coherent structures is 30% of centreline velocity (60% of top-hat velocity)
- Motion of visible coherent structures on the edge of a plume can be used to predict the buoyancy (15%) and volume (5%) in a pure plume
- Significant differences in plume behaviour when eddies are present or absent
  - 1 larger vertical velocities in the external flow
  - 2 larger velocities into the plume
  - 3 larger external vertical volume flux
- Larger average width of buoyancy compared with velocity due to presence of engulfed fluid